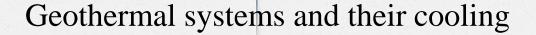
# Modeling thermal evolution caused by thermal water production and injection wells

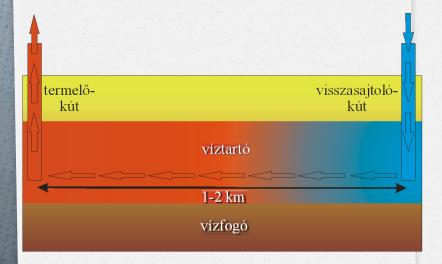
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- production time
- geometry of the wells, distance
- o effects of 30 years production



What?

How?

Equation of subsurface water flow+ heat transport

Numerical modeling, finite element method (Feflow 6.0x)

### **Equations**

#### Darcy's Law

Governing equation of water flow in porous medium

$$u = -K\nabla h$$

 $u = -K\nabla h$  K - hydraulic conductivity [m/s]

 $\underline{\mathbf{u}}$  - Darcy velocity  $[\mathbf{m}^3/\mathbf{m}^2\,\mathbf{s}] = [\mathbf{m}/\mathbf{s}]$ 

h - hydraulic head

$$h = \frac{p - p_{hidr}}{\rho g}$$

#### **Continuity equation**

$$s_0 \frac{\partial h}{\partial t} = K \nabla^2 h + Q$$

 $s_0$ - specific storage [1/m]

Q - source  $[m^3/m^3s]$ 

t - time [s]

#### Heat transport

$$c_{p\,m}\rho_m\,\frac{\partial T}{\partial t} = c_{p\,f}\rho_f\,\underline{u}\nabla T + \lambda\nabla^2 T + Q_T$$

1: change of heat energy, 2: advection, 3: conduction, 4: source

T – temperature [°C]

 $\lambda$  – thermal conductivity [W/m°C]

Q<sub>T</sub> – heat source [W/m3]

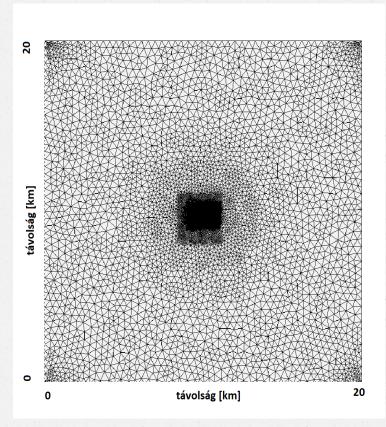
 $c_p$  – heat capacity [J/kg°C],  $\rho$  – density [kg/m<sup>3</sup>]

#### Numerical solution:

Calculation of  $h \longrightarrow \text{Darcy's Law -u} \longrightarrow \text{heat transport}$ 



- The model area consists of finite elements and nodes
- Number of nodes 
   — number of equation
- Initial and boundary conditions
- Calculating: hydraulic head, temperature
- Time-iteration with Adams-Bashforth method (hydraulic head, T change ↔ time-step size )
- model geometry x=20 km, y=20 km, z=3,5 km



*Used mesh geometry* 





## Comparison of numerical solution with analitical solution

#### Point source

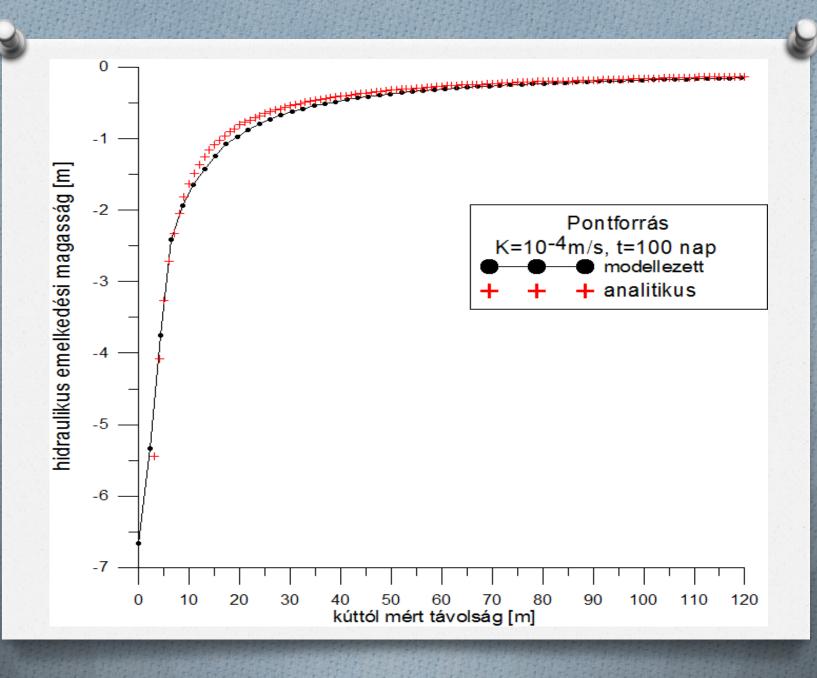
- 1. Hydraulic head
- depending on the time of production
- 2. Temperature

Eqaution of hydraulic head:

$$\frac{\partial h}{\partial t} = \frac{K}{s_0} \left( \frac{\partial^2 h}{\partial r^2} + \frac{2}{r} \frac{\partial h}{\partial r} \right) + \frac{Q_\rho}{s_0}$$

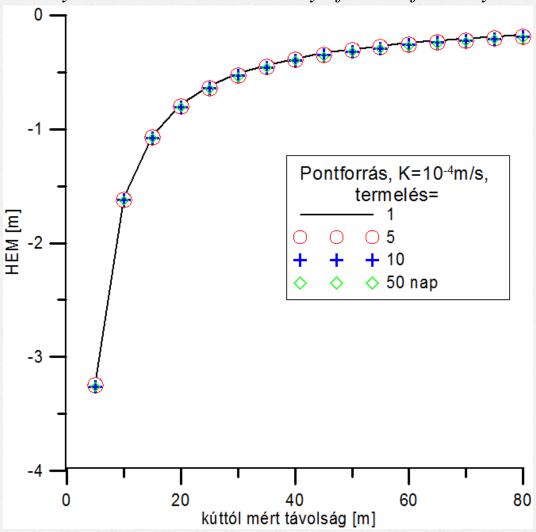
initial and boundary condition:

- $h(0,r) = h_0$
- The model boundary- $h_0$ :  $\lim_{r\to\infty} h(t,r) = h_0$
- the pumping rate is constant :  $\lim_{r\to 0} \left(r\frac{\partial h}{\partial r}\right) = \frac{Q}{4\pi\frac{K}{s_0}}$



Analytic solution of hydraulic head as a function of production time.

Hydraulic head is stationary after the first day.



#### Point source

#### 2. Temperature

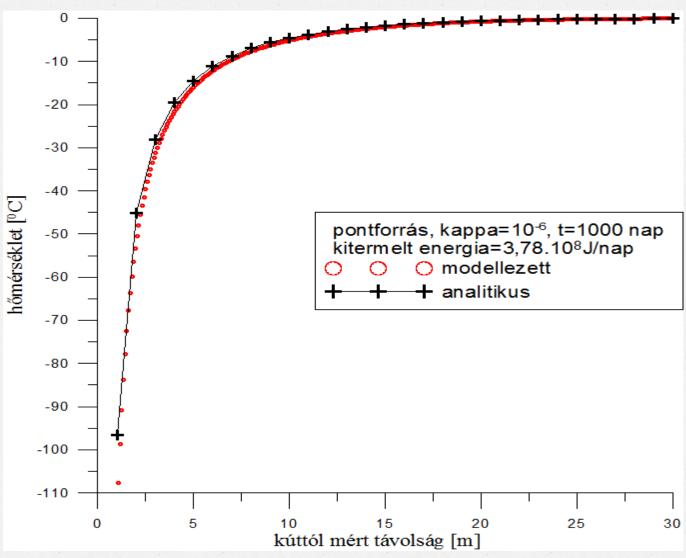
Comparison of analytical and numerical calculation

Eqaution of temperature:

$$\frac{\partial T}{\partial t} = \kappa \left( \frac{\partial^2 T}{\partial r^2} + \frac{2}{r} \frac{\partial T}{\partial r} \right) + \frac{Q_T}{c\rho}$$

initial and boundary condition:

- initial temperature : T(0, r) = 0
- amount of heat produced at r=0  $Q_T=0$
- $Q_T = 3.78.10^8 \text{J/day}$
- Thermal diffusivity:  $\kappa = 10^{-6} \,\mathrm{m}^2/\mathrm{s}$



heat production:  $Q_T = 3.78.10^8 \text{J/day}$ 

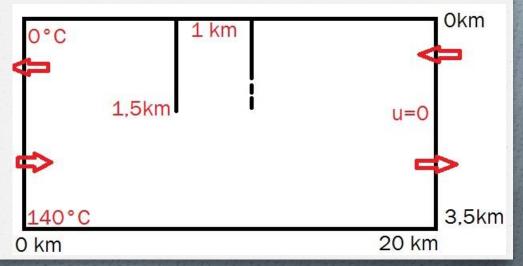
#### Modeling production

#### Initial and boundary condition: and injection wells

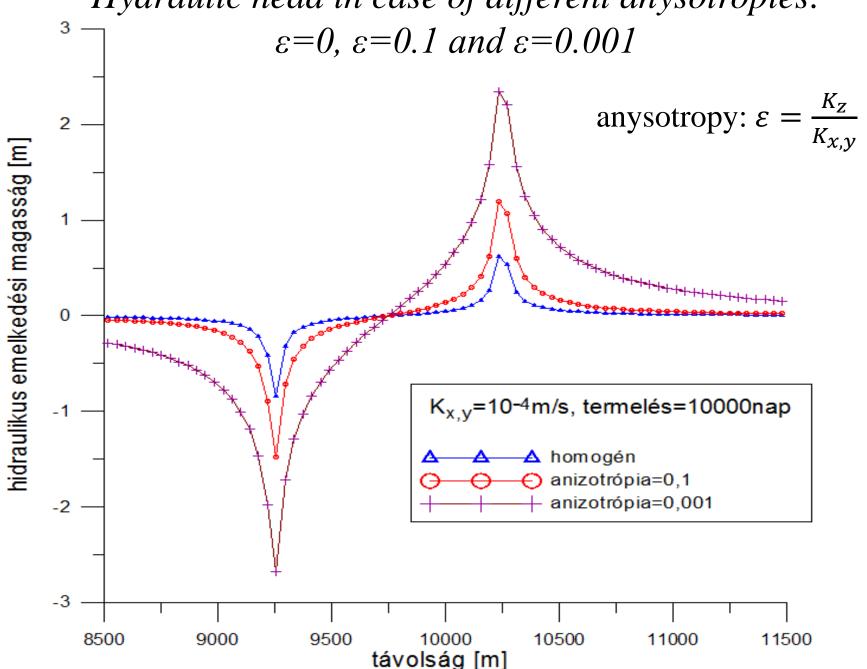
- initial hydraulic head: h(x, y, z, t = 0) = 0
- amount of production and injection: 2000 m<sup>3</sup>/day
- Temperature of produced water: 60°C
- Temperature of injected water: 20°C

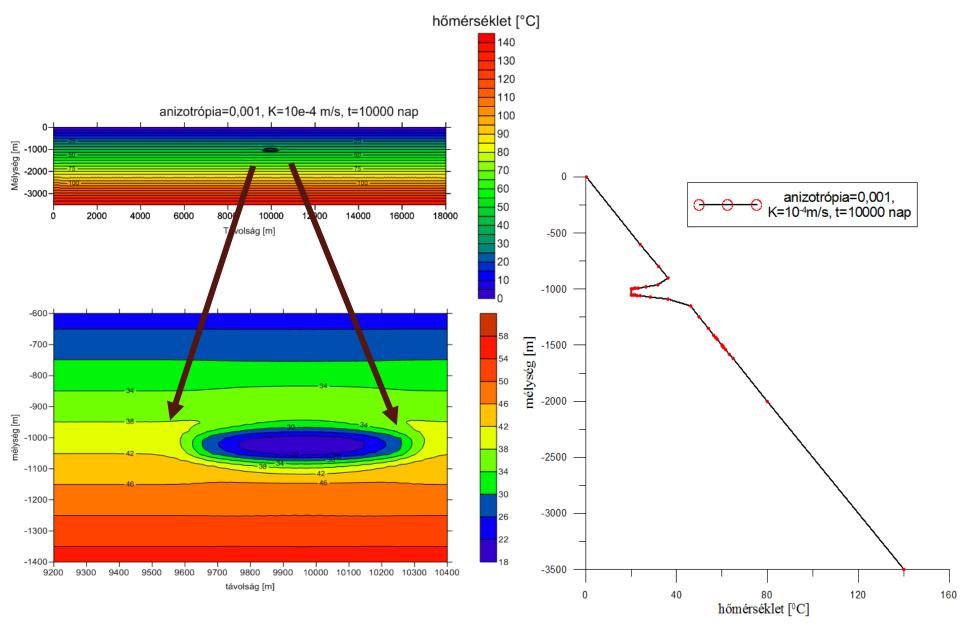
#### Two case-studies:

- injection into the same layer (1500-1550 m)
- into a different layer (1000-1050 m)



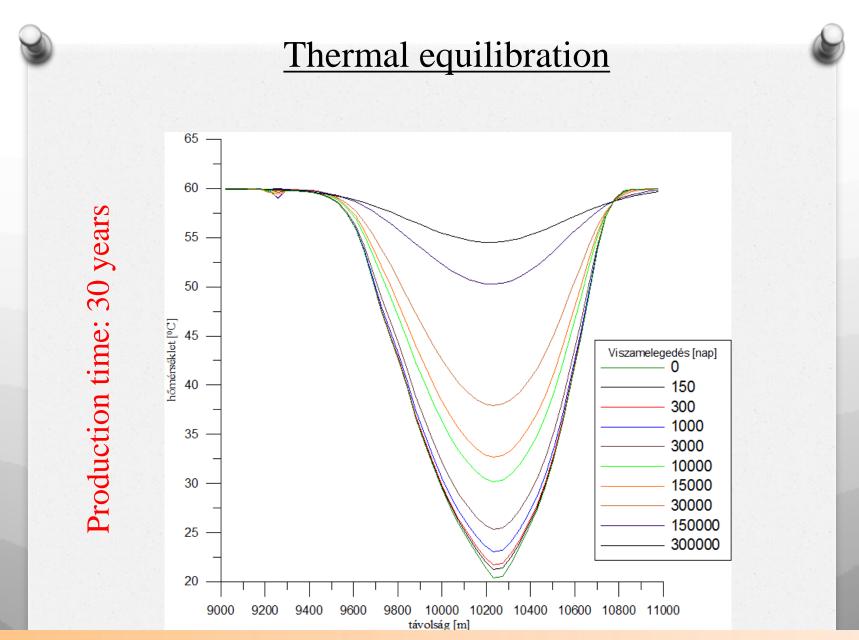
Hydraulic head in case of different anysotropies:





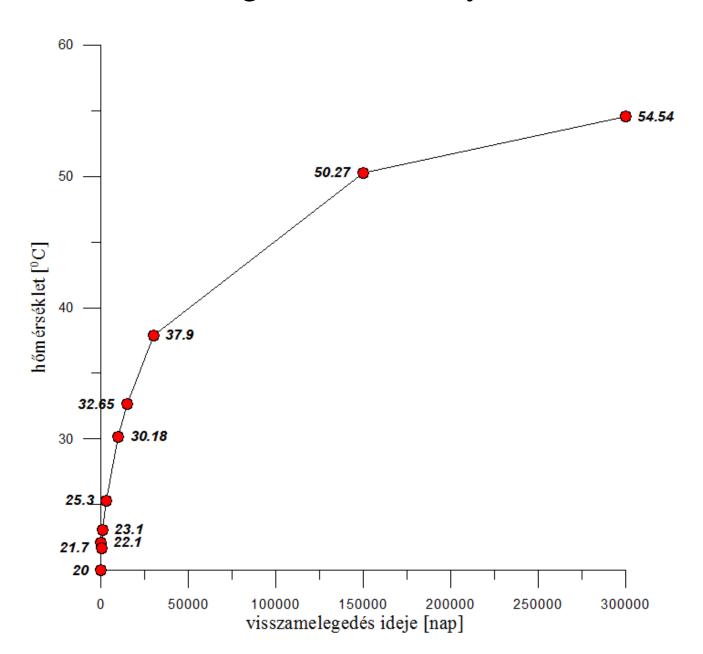
Enlarged vertical section of a cooled-down environment around an injection well

Temperature-depth profile at the injection well



300000 days (1000 years) are needed to reach the 90 % of the original temperature.

#### Warming of the cold layer



#### **Summary**

- © Comparision of analytical and numerical solutions
- ② 30 years of production does not have effect on the temperature of the produced water in case of wells located 1 km from each other
- 1000 years of reheating

# Thank you for your attention!